

still, the present application is one of five co-pending applications that were filed simultaneously and with essentially common disclosures. Three of the five co-pending cases were filed free of any typographical errors. For instance, all substituted symbols (in particular, symbols in connection with the description of FIG. 1d) are supported by co-pending application 10/050,529, having at least one common inventor with the present application. Applicants respectfully submit that this amendment adds no new matter, is fully supported by the instant and priority disclosures, and merely corrects typographical errors and, therefore, should be entered.

If the Examiner believes that a telephone conference or interview would advance prosecution of this application in any manner, the undersigned stands ready to conduct such a conference at the convenience of the Examiner.

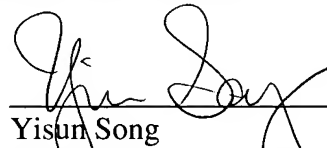
It is believed that no fees are due in connection with the filing of this Preliminary Amendment. In the event it is determined that a fee is necessary to maintain the pendency of this application, the Commissioner is hereby authorized to charge or credit the undersigned's Deposit Account No. 50-0206.

Respectfully submitted,

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Date: April 18, 2002

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**ATTACHMENT A - REVISIONS TO SPECIFICATION**

At page 12, line 16, delete “!” and insert --±--;

line 17, delete “!” and insert --±;

line 19, delete “!” and insert --±--.

At page 13, line 2, delete “ $\theta + \alpha$ ” and insert -- $\gamma + \delta$ --;

line 8, delete “ $\theta$ ” and insert -- $\gamma$ --;

line 10, delete “ $\alpha$ ” and insert -- $\delta$ --;

At page 16, line 1, delete “ $\alpha < \theta$ ” and insert -- $\alpha < \beta$ --;

line 5, delete “ $\alpha$ ” and insert -- $\alpha$ --;

line 5, delete “ $\theta$ ” and insert -- $\beta$ --.

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At page 18, line 13, delete “ $\exists$ ”(both occurrences) and insert -----;

line 14, delete “ $\exists$ ”(both occurrences) and insert -----;

line 15, delete “ $\uparrow$ ” and replace with -----;

At page 20, line 10, delete “ $\exists$ ”(both occurrences) and insert -----;

line 11, delete “ $\exists$ ”(both occurrences) and insert -----;

line 13, delete “ $\uparrow$ ” and replace with -----;

At page 22, line 3, delete “ $\theta$ ” and insert -- $\gamma$ --;

line 4, delete “ $\alpha$ ” and insert -- $\delta$ --;

At page 24, line 4, delete “ $\alpha < \theta$ ” and insert -- $\alpha < \beta$ --;

line 7, delete “ $\theta$ ” and insert -- $\gamma$ --;

line 8, delete “ $\alpha$ ” and insert -- $\delta$ --.



At page 29, line 15, delete “{” and insert --≅--.

At page 44, line 26, delete “③” and insert --μ--.

## APPENDIX B - SPECIFICATION AFTER AMENDMENTS

Page 12, second paragraph, lines 14-26; and page 13, lines 1-8, replace these paragraphs in their entirety with the following:

FIG. 1d is an example of a timing diagram of an activation sequence. As illustrated, STUR may initiate Cr, lasting a duration of  $t_{cr}$ , which has a nominal value of 1 second with  $\pm 20$  millisecond tolerance. Time from the end of Cr to a beginning of Sc is represented by  $t_{crsc}$ , which has a nominal value of 500 millisecond with  $\pm 20$  millisecond tolerance. After a time  $t_{crsc}$ , STUC may initiate Sc. Time from the end of Cr to a beginning of Sr is represented by  $t_{crsr}$ , which has a nominal value of 1.5 second with  $\pm 20$  millisecond tolerance. After a time  $t_{crsr}$ , STUR may initiate Sr. After Sc, STUC may initiate Tc. After Sr, STUR may initiate Tr. After Tc, STUC may initiate Fc. At approximately the same time, Data<sub>c</sub> and Data<sub>r</sub> may be initiated by STUC and STUR, respectively. Time from the beginning of Cr to the beginning of Data<sub>r</sub> is represented by  $t_{Actdata}$ , which has a nominal value of 15 seconds.

If the SNR is calculated in the time domain, one method to determine PBO is according to the equations shown below.

$$SNR_{dB} = 10\log_{10} \left( \frac{P_{signal+noise}}{P_{noise}} \right) = 10\log_{10} \left( \frac{\sum_{n=0}^{M-1} |s(n) + w(n)|^2}{\sum_{n=0}^{M-1} |w(n)|^2} \right) \quad (1)$$

$$PBO_{dB} = SNR_{dB} - (\gamma + \delta + SNR_{min}) \quad (2)$$

$s(n) = n^{th}$  sample of the received signal

$w(n) = n^{th}$  sample of the received noise

$M$  = window length in samples used to compute average

$P_{signal+noise}$  = power of signal + noise

$P_{noise}$  = power of noise only

where  $\gamma$  represents a required margin in dB ( $\geq 0$  dB, example: G.SHDSL Annex B margin is 6 dB);  $SNR_{min}$  represents a minimum SNR in dB needed to obtain the specified BER, and  $\delta$  represents an implementation loss in dB.

**Page 15, second paragraph, lines 8-20; and page 16, lines 1-7, replace this paragraph in its entirety with the following:**

Using the geometric mean, a SNR of the channel may be computed using the following:

$$SNR \equiv \left[ \prod_{k=\alpha}^{\beta} \frac{|Y(k) - \hat{W}(k)|^2}{|W(k)|^2} \right]^{\frac{1}{\beta-\alpha+1}} \quad (6)$$

$$SNR \equiv 10 \log_{10} \left[ \prod_{k=\alpha}^{\beta} \frac{|Y(k) - \hat{W}(k)|^2}{|W(k)|^2} \right]^{\frac{1}{\beta-\alpha+1}} = \frac{10}{\beta-\alpha+1} \sum_{k=\alpha}^{\beta} \log_{10} \left[ \frac{|\hat{S}(k)|^2}{|W(k)|^2} \right] \quad (7)$$

which may be rewritten in the following manner to filter cells with negative or zero SNR

$$D'_k = \log_{10} \left[ \frac{|\hat{S}(k)|^2}{|W(k)|^2} \right] \quad (8)$$

$$D_k = \begin{cases} D'_k & D'_k > 0 \\ 0 & \text{otherwise} \end{cases} \quad (9)$$

$$SNR_{dB} = \frac{10}{\beta-\alpha+1} \left( \sum_{k=\alpha}^{\beta} D_k \right) \quad (10)$$

where  $0 < \alpha < \beta < N-1$ ;  $\hat{S}(k)$  represents an estimate of  $k^{\text{th}}$  frequency sub-band of a received signal spectrum;  $\hat{W}(k)$  represents an estimate of  $k^{\text{th}}$  frequency sub-band of a received noise spectrum;  $Y(k)$  represents a  $k^{\text{th}}$  frequency sub-band of signal plus noise spectrum;  $\alpha$  represents a starting sub-band;  $\beta$  represents an ending sub-band;  $D_k$  represents one or more sub-bands with SNR greater than zero;  $D'_k$  represents SNR for  $k^{\text{th}}$  sub-band.

**Page 18, first paragraph, lines 3-17, replace this paragraph in its entirety with the following:**

Equation (15) is described in “The Fast Fourier Transforms and it’s Applications” by E. Oran Brigham –1988 – equation 6.16, page 97.

The first cosine and sine terms may be found using the equations below.

$$R_0 = \cos\left(\frac{4\pi}{N_{real}}\right) \quad (16)$$

$$I_0 = -\sin\left(\frac{4\pi}{N_{real}}\right) \quad (17)$$

where

$N_{real}$  = real FFT size

$R_0$  = zero<sup>th</sup> sample of real part of exponential weight

$I_0$  = zero<sup>th</sup> sample of imaginary part of exponential weight

The equations to recursively compute the transform weights are given below:

$$R_m = R_0 \cdot R_{m-1} - I_0 \cdot I_{m-1} \quad (18)$$

$$I_m = I_0 \cdot R_{m-1} + R_0 \cdot I_{m-1} \quad (19)$$

where  $m = 1, 2, \dots, \frac{N_{real}}{4}$

$R_m$  =  $m^{\text{th}}$  sample of real part of exponential weight

$I_m$  =  $m^{\text{th}}$  sample of imaginary part of exponential weight

**Page 20, first paragraph, lines 7-13, replace this paragraph in its entirety with the following:**

Equations (18) and (19) may be modified slightly and then used with the above initializers to compute the new weights.

$$R_m = R_0 \cdot R_{m-1} - I_0 \cdot I_{m-1} \quad (28)$$

$$I_m = I_0 \cdot R_{m-1} + R_0 \cdot I_{m-1} \quad (29)$$

where  $m = 1, 2, \dots, \frac{N_{real}}{2}$

**Page 21, last paragraph, lines 22-27; and page 22, lines 1-4, replace this paragraph in its entirety with the following:**

If the SNR is calculated in the time domain, a method to compute the capacity may include measuring the silence power (noise),  $P_{noise}$ , and then the received power (signal + noise),  $P_{signal+noise}$ , and finding the capacity,  $C$ , using the equation below.

$$C = B \log_2 \left( 1 + \frac{P_{signal}}{P_{noise} 10^{\frac{(\Gamma - G + \gamma + \delta)}{10}}} \right) = B \log_2 \left( 1 + \frac{SNR}{10^{\frac{(\Gamma - G + \gamma + \delta)}{10}}} \right) \frac{bits}{second} \quad (30)$$

where  $\Gamma$  represents a gap from a theoretical channel capacity for PAM signals, in dB;  $G$  represents a coding gain of a Trellis decoder in dB;  $B$  represents a transition bandwidth;  $\gamma$  represents a required margin in dB (e.g., G.SHDSL Annex B margin is approximately 6 dB); and  $\delta$  represents an implementation loss in dB.

**Page 23, last paragraph, lines 23-27; and page 24, lines 1-9, replace this paragraph in its entirety with the following:**

Starting with equation (30) above, an overall capacity may be determined by summing capacities for each individual sub-band as shown by equation (33) below.

$$\begin{aligned}
C &\equiv B_s \sum_{k=\alpha}^{\beta} \log_2 \left( 1 + \frac{|Y(k) - \hat{W}(k)|^2}{|\hat{W}(k)|^2 10^{\frac{(\Gamma-G+\gamma+\delta)}{10}}} \right) \\
&= B_s \sum_{k=\alpha}^{\beta} \log_2 \left( \frac{|\hat{W}(k)|^2 10^{\frac{(\Gamma-G+\gamma+\delta)}{10}} + |Y(k) - \hat{W}(k)|^2}{|\hat{W}(k)|^2 10^{\frac{(\Gamma-G+\gamma+\delta)}{10}}} \right) \\
&= B_s \left( \sum_{k=\alpha}^{\beta} \log_2 \left( |\hat{W}(k)|^2 10^{\frac{(\Gamma-G+\gamma+\delta)}{10}} + |\hat{S}(k)|^2 \right) - \sum_{k=\alpha}^{\beta} \log_2 \left( |\hat{W}(k)|^2 10^{\frac{(\Gamma-G+\gamma+\delta)}{10}} \right) \right) \quad (33)
\end{aligned}$$

where  $B_s = \frac{B}{(\beta - \alpha + 1)}$ ;  $0 < \alpha < \beta < N-1$ ;  $B_s$  represents a sub-band width in Hz;  $\hat{S}(k)$  represents an estimated “signal only” power;  $\Gamma$  represents a gap from a theoretical channel capacity for PAM signals, in dB;  $G$  represents a coding gain of a Trellis decoder in dB;  $\gamma$  represents a required margin in dB (e.g., G.SHDSL Annex B margin is approximately 6dB);  $\delta$  represents an implementation loss in dB,  $\alpha$  represents an index of a first sub-band and  $\beta$  represents an index of a last sub-band.

**Page 29, fourth paragraph, lines 12-22, replace this paragraph in its entirety with the following:**

As shown in FIG. 7, an output of the precoder 710 may have an approximately flat power spectrum. Keeping this in mind while tracing the signal paths in the above block diagram, the following may apply:

$$X(f) \cong K = \text{constant} \quad (37)$$

$$Y(f) = X(f)H_{txf}(f)H_{ec}(f) + T_f(f)H_c(f) + W(f) \quad (38)$$

$$Z(f) = X(f)H_{dec}(f) \quad (39)$$

$$\begin{aligned}
E(f) &= Y(f) - Z(f) = [H_{txf}(f)H_{ec}(f) - H_{dec}(f)]X(f) + T_f(f)H_c(f) + W(f) \\
&= [H_{txf}(f)H_{ec}(f) - H_{dec}(f)]K + T_f(f)H_c(f) + W(f) \quad (40)
\end{aligned}$$



where  $R_e(f)$  is defined as  $[H_{tx}(f)H_{ec}(f) - H_{dec}(f)]K$  wherein  $R_e(f)$  represents residual echo spectrum, then  $E(f) = R_e(f) + T_f(f)H_c(f) + W(f)$ .

**Page 44, fourth paragraph, lines 23-30 and page 45, line 1, replace this paragraph in its entirety with the following:**

The optimum shift points may be determined by software. The following table lists the gear-shift point in samples and the right shift (e.g., power of two) division of the weights. These gears may be used in the initial training. While in steady state, a single gear may be used and may be approximately  $\frac{1}{2}$  the smallest  $\mu$  in the table.

Gear#	0	1	2	3	4	5
Samples	2000	598	1427	3188	7241	15000
Right Shift	3	4	5	6	7	8